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(54) **Equipment for and methods of locating the position of a fault on a power transmission line.**

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IEEE TRANS. ON POWER APPARATUS AND SYSTEMS, vol. PAS-101, nos. 8/9, August-September 1982, pages 2892-2898, IEEE, New York, US; T. TAKAGI et al.: "Development of a new type fault locator using the one-terminal voltage and current data"

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PATENT ABSTRACTS OF JAPAN, vol. 12, no.

125 (P-691)[2972], 19th April 1988; & JP-A-62 249 078 (CHUBU ELECTRIC POWER)
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(73) Proprietor: **GEC ALSTHOM LIMITED**
Mill Road
Rugby Warwickshire CV21 1BD(GB)

(72) Inventor: **Johns, Allan Thomas**
25 Whittington Road
Westlea Down Swindon SN5 7DF(GB)

(74) Representative: **Pope, Michael Bertram Wингate**
The General Electric Company, p.l.c.
GEC Patent Department
Waterhouse Lane
Chelmsford, Essex CM1 2QX (GB)

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Description

This invention relates to equipment for and methods of locating the position of a fault on a power transmission line.

5 Satisfactory operation of known forms of such equipment, for example those using impedance to fault measuring techniques or adaptations thereof, relies on one or more of a number of assumptions which make them inaccurate in certain circumstances. The main assumptions made are as follows: that the transmission line conductors are ideally transposed; that the parameters of the network in which the transmission line is connected are known and constant; that the fault type can be determined; that shunt 10 capacitance of the line can be neglected; and that the phase of the current in the fault path can be determined.

It is an object of the present invention to provide an equipment for and method of locating the position of a fault on a power transmission line whose operation does not depend on any of the above assumptions.

According to a first aspect of the present invention there is provided an equipment for locating the 15 position of a fault on a power transmission line between a first and a second end of said line comprising: first means for deriving first and second signals representative respectively of the voltage V_S and current I_S at said first end; second means for deriving third and fourth signals representative respectively of the voltage V_R and current I_R at said second end; and means for calculating the position of the fault utilising said first, second, third and fourth signals and equations of the form:

$$\begin{aligned} 20 \quad X_f &= A_S V_S - B_S I_S ; \text{ and} \\ X_f &= A_R V_R - B_R I_R , \end{aligned}$$

where X_f is the fault voltage or current, A_S is a first transmission parameter of the line between the fault and 25 said first end, B_S is a second transmission parameter of the line between the fault and said first end, A_R is a first transmission parameter of the line between the fault and said second end, and B_R is a second transmission parameter of the line between the fault and said second end, each said transmission parameter being dependent upon the distance of the fault along the transmission line from a said end of the line.

30 In one particular equipment according to the invention where said power transmission line is a multi-phase power transmission line; said first and second means derive a set of said first, second, third and fourth signals in respect of each phase of said transmission line; and said means for calculating includes means for transforming said signals to produce corresponding sets of decoupled signals V_{Sn} , I_{Sn} , V_{Rn} , I_{Rn} and means for utilising each set of said decoupled signals in equations of the form:

$$\begin{aligned} 35 \quad X_{fn} &= A_{Sn} V_{Sn} - B_{Sn} I_{Sn} ; \text{ and} \\ X_{fn} &= A_{Rn} V_{Rn} - B_{Rn} I_{Rn} , \end{aligned}$$

where n indicates the relevant said set.

40 According to a second aspect of the present invention there is provided a method of locating the position of a fault on a power transmission line between a first and a second end of said line comprising the steps of: deriving first and second signals representative respectively of the voltage V_S and current I_S at said first end; deriving third and fourth signals representative respectively of the voltage V_R and current I_R at said second end; and calculating the position of the fault utilising said first, second, third and fourth signals 45 and equations of the form:

$$\begin{aligned} X_f &= A_S V_S - B_S I_S ; \text{ and} \\ X_f &= A_R V_R - B_R I_R , \end{aligned}$$

50 where X_f is the fault voltage or current, A_S is a first transmission parameter of the line between the fault and said first end, B_S is a second transmission parameter of the line between the fault and said first end, A_R is a first transmission parameter of the line between the fault and said second end, and B_R is a second transmission parameter of the line between the fault and said second end, each said transmission parameter being dependent upon the distance of the fault along the transmission line from a said end of the line.

55 In one particular method according to the invention where said power transmission line is a multi-phase power transmission line; the steps of deriving said first, second, third and fourth signals comprise deriving a set of said first, second, third and fourth signals in respect of each phase of said transmission line; and the

step of calculating includes transforming said signals to produce corresponding sets of decoupled signals V_{Sn} , I_{Sn} , V_{Rn} , I_{Rn} and utilising each set of said decoupled signals in equations of the form:

$$X_{fn} = A_{Sn}V_{Sn} - B_{Sn}I_{Sn}; \text{ and}$$

$$5 \quad X_{fn} = A_{Rn}V_{Rn} - B_{Rn}I_{Rn},$$

where n indicates the relevant set.

EP-A-0230801 discloses fault locating equipment which uses voltage and current data from both ends of the line. The equipment utilises two equations for the fault voltage, equations (1) and (2) at lines 37 and 10 38 on page 3 of EP-A-0230801. These equations are distinguished from the two equations specified in each of Claims 1 and 6 of the present application. In the equations of EP-A-0230801, transmission line parameters A_S and A_R of the equations of Claim 1 are set to unity. In other words the coefficient of each of ΔV_A and ΔV_B in the equations of EP-A-0230801 is unity, whereas in the equations of Claim 1 the coefficient of each of V_S and V_R is a transmission line parameter dependent upon the position of the fault. 15 Thus, in essence, EP-A-0230801 makes the assumption that the transmission line is non-distributed, whereas the invention of the present application does not.

The invention will now be further explained and, one equipment for and method of locating the position of a fault on a power transmission line in accordance with the invention described by way of example, with reference to the accompanying drawings in which:

- 20 Figure 1 is a diagram illustrating a two port network;
 Figure 2 is a schematic diagram of a power transmission line having a fault;
 Figure 3 is a schematic diagram of the equipment; and
 Figure 4 is a block schematic diagram showing the part of the equipment at one end of the transmission line in greater detail.
 25 The invention makes use of the well known two port network equation. The two port network equation relates the voltage and current at one port of a two port network to the voltage and current at the other port, as follows:

$$30 \quad \begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A_1B_1 \\ A_2B_2 \end{bmatrix} \begin{bmatrix} V_2 \\ I_2 \end{bmatrix} \quad (1),$$

35 where, as illustrated in Figure 1, V_1 and I_1 are the voltage and current respectively at one port of a two port network 1, V_2 and I_2 are the voltage and current respectively at the other port of the two port network 1, and A_1 , A_2 , B_1 and B_2 are the parameters, i.e. transfer functions, of the two port network 1. Multiplying out the matrices of equation (1) gives:

$$40 \quad V_1 = A_1V_2 + B_1I_2 \quad (2)$$

$$\text{and } I_1 = A_2V_2 + B_2I_2 \quad (3).$$

The invention resides in the application of the two port network equation to the or each phase of a 45 power transmission line having a fault in respect of the parts of the line on either side of the fault. Thus, referring to Figure 2, application of equation (2) to parts 3 and 5 of a power transmission line 7 on either side of a fault 9 produces an equation:

$$V_f = A_SV_S - B_SI_S \quad (4)$$

50 for part 3, and produces an equation:

$$V_f = A_RV_R - B_RI_R \quad (5)$$

55 for part 5; where: V_f is the fault voltage; V_S and I_S are the voltage and current respectively at the end 11 of the part 3 of the transmission line 7 remote from the fault 9; V_R and I_R are the voltage and current respectively at the end 13 of the part 5 of the transmission line 7 remote from the fault 9; A_S and B_S are first and second transmission line parameters between the fault 9 and the end 11; and A_R and B_R are first and

second transmission line parameters between the fault 9 and the second end 13. From transmission line theory:

$$\begin{aligned} A_S &= \cosh(Tx) \\ 5 \quad B_S &= Z_0 \sinh(Tx) \\ A_R &= \cosh(T(L-x)) \\ B_R &= Z_0 \sinh(T(L-x)) \quad (6). \end{aligned}$$

where T is the propagation constant of the line 7, x is the distance of the fault 9 along the transmission line 7 from the end 11, Z_0 is the characteristic impedance of the line 7 and L is the total length of the line 7 between the ends 11 and 13.

Equating the right-hand sides of equations (4) and (5) and substituting for A_S , B_S , A_R and B_R from equations (6) gives:

$$15 \quad \cosh(Tx)V_S - Z_0 \sinh(Tx)I_S = \cosh(T(L-x))V_R - Z_0 \sinh(T(L-x))I_R$$

Expanding $\cosh(T(L-x))$ and $\sinh(T(L-x))$ gives:

$$16 \quad \cosh(Tx)V_S - Z_0 \sinh(Tx)I_S = V_R(\cosh(TL)\cosh(Tx) - \sinh(TL)\sinh(Tx)) - I_RZ_0(\sinh(TL)\cosh(Tx) - \cosh(TL)\sinh(Tx)).$$

Rearranging gives:

$$- \cosh(Tx)(V_R\cosh(TL) - I_RZ_0\sinh(TL) - V_S) = \sinh(Tx)(I_RZ_0\cosh(TL) - V_R\sinh(TL) + I_SZ_0).$$

25 Therefore:

$$30 \quad \tanh(Tx) = \frac{- (V_R\cosh(TL) - I_RZ_0\sinh(TL) - V_S)}{I_RZ_0\cosh(TL) - V_R\sinh(TL) + I_SZ_0}$$

35 Therefore:

$$40 \quad x = \frac{\tanh^{-1}(-Q/P)}{T} \quad (7),$$

where:

$$45 \quad P = I_RZ_0\cosh(TL) - V_R\sinh(TL) + I_SZ_0 \quad (8)$$

and:

$$Q = V_R\cosh(TL) - I_RZ_0\sinh(TL) - V_S \quad (9).$$

50 Hence, if the values of V_S , I_S , V_R , I_R , Z_0 , T and L are known, the distance x of the fault 9 along the transmission line 7 from the end 11 can be calculated from equations (7), (8) and (9). V_S , I_S , V_R and I_R can be measured at each end of the line and Z_0 , T and L will be known for a given transmission line.

It is to be noted that equations (7), (8) and (9) hold irrespective of the type of the fault 9 and are indeterminate for a fault free healthy line. Furthermore, equations (7), (8) and (9) are independent of the fault path which may therefore be non-linear and still not affect the calculation of x . T and Z_0 cater for the non-transposition and shunt capacitance of the line and are not affected by the parameters of the network in which the transmission line is connected.

One example of an equipment for carrying out the method according to the invention will now be described with reference to Figure 3.

The equipment comprises, at each of the two ends 11 and 13 of the line 7, a voltage sensor 15A or 15B and current sensor 17A or 17B, for measuring the voltage V_S or V_R and current I_S or I_R at that end 11 or 13 of the line 7, an analogue to digital (A/D) converter 19A or 19B for converting the analogue signals output by the voltage and current sensors 15A, 17A or 15B, 17B into digital form, a microprocessor 21A or 21B which receives these digital signals and a display 23A or 23B. The line 7 is shown as interconnecting two power transmission systems R and S. The microprocessors 21A and 21B are interconnected so that each microprocessor 21A or 21B receives not only the digital voltage and current signals from the end at which it is situated, but also the digital voltage and current signals from the other end of the line 7. Each microprocessor 21A or 21B can therefore calculate x as defined by equations (7), (8) and (9) using the values of V_S , I_S , V_R and I_R input to it and the known values of Z_0 , T and L . The value of x is displayed on each of the displays 23.

Where the line 7 is a multiphase transmission line, the calculations are performed in respect of each phase of the transmitted power. However, in the case of a multiphase line the problem arises that the different phases will normally not be decoupled.

To overcome this problem a modal component transformation may be used, as described in an article by L.M.Wedepholt entitled 'Application of matrix methods to the solution of travelling-wave phenomena in polyphase systems' published in December 1963 in Proc. IEE, Vol 110, No 12, at pages 2200 to 2212.

To this end the microprocessors 21A and 21B are arranged to multiply the voltage and current quantities V_S , I_S or V_R , I_R for each phase by an appropriate transformation matrix to produce corresponding sets of decoupled quantities V_{Sn} , I_{Sn} or V_{Rn} , I_{Rn} where n is 1, 2 etc. up to the number of phases in the system. These decoupled quantities are then utilised in respect of each phase of the line 7 in equations of the form:

$$V_{In} = A_{Sn} V_{Sn} - B_{Sn} I_{Sn} \quad (10)$$

and

$$V_{Rn} = A_{Rn} V_{Rn} - B_{Rn} I_{Rn} \quad (11),$$

where A_{Sn} , B_{Sn} , A_{Rn} and B_{Rn} are the model line parameters and

$$\begin{aligned} A_{Sn} &= \cosh(T_n x) \\ 35 \quad B_{Sn} &= Z_{On} \sinh(T_n x) \\ A_{Rn} &= \cosh(T_n(L-x)) \\ B_{Rn} &= Z_{On} \sinh(T_n(L-x)) \quad (12), \end{aligned}$$

where T_n are the modal propagation constants of the line and Z_{On} are the characteristic modal impedances of the line. Equations (10), (11) and (12) are then worked in the same way as equations (4), (5) and (6) above to obtain the distance x of the fault along the line 7 from the end 11, as in equations (7), (8) and (9) above; that is:

$$45 \quad x = \frac{\tanh^{-1}(-Q_n/P_n)}{T_n} \quad (13),$$

50 where:

$$P_n = I_{Rn} Z_{On} \cosh(T_n L) - V_{Rn} \sinh(T_n L) + I_{Sn} Z_{On} \quad (14)$$

and

$$55 \quad Q_n = V_{Rn} \cosh(T_n L) - I_{Rn} Z_{On} \sinh(T_n L) - V_{Sn} \quad (15).$$

One particular form of the equipment at each end of the line 7 will now be described in greater detail with reference to Figure 4. The equipment is for use with a three-phase transmission line. The three phase voltage and current signals V_a , V_b , V_c , I_a , I_b and I_c from line transformers (not shown) are fed, via an isolation transformer 33 and filters 35 for extracting the power frequency phase information, to a multiplexer 37. The output of the multiplexer 37 is then passed via a sample and hold gate 39 to an A/D converter 41. The resultant digitised signals are stored in a cyclic buffer in a random access memory 43 of a microprocessor 44 by a direct memory access unit 45. An input/output unit 46 is sampled continuously until a start signal indicating occurrence of fault is received from a line protection equipment, typically a distance relay, after which the process of sampling the phase voltage and current signals V_a , V_b , V_c , I_a , I_b , I_c continues until post fault data has been captured. The microprocessor 44 then carries out the necessary calculations. A keypad and alpha numeric display 47 are used to display and transfer the modal voltages and currents, to display the final distance to fault result calculated by the microprocessor and to enter the line parameters for storage in an electrically erasable programmable read only memory 49.

It will be understood that if the line 7 is a multi-circuit line there will be a set of modal components for each phase and each circuit. Thus for a single circuit three-phase line n will have values 1, 2 and 3 and for a double circuit three-phase line will have values 1 to 6.

It will be further understood that transformations other than a modal component transformation may be used for decoupling purposes in equipment and methods according to the invention. For example, the well known symmetrical component transformation might be used, for example, if the transmission line conductors were known to be ideally transposed.

It is also pointed out that whilst in the above explanation of the invention and in the equipment and method described by way of example, use of the voltage equation (2) is described, the current equation (3) could equally well be used.

25 Claims

1. An equipment for locating the position of a fault (9) on a power transmission line (7) between a first (11) and a second (13) end of said line (7) comprising: first means (15A,17A,19A) for deriving first and second signals representative respectively of the voltage V_s and current I_s at said first end (11); second means (15B,17B,19B) for deriving third and fourth signals representative respectively of the voltage V_R and current I_R at said second end (13); and means (21A,21B) for calculating the position of the fault (9) utilising said first, second, third and fourth signals and equations of the form:

$$X_f = A_s V_s - B_s I_s ; \text{ and}$$

$$X_f = A_R V_R - B_R I_R ,$$

where X_f is the fault voltage or current, A_s is a first transmission parameter of the line (7) between the fault (9) and said first end (11), B_s is a second transmission parameter of the line (7) between the fault (9) and said first end (11), A_R is a first transmission parameter of the line (7) between the fault (9) and said second end (13), and B_R is a second transmission parameter of the line (7) between the fault (9) and said second end (13), each said transmission parameter being dependent upon the distance of the fault (9) along the transmission line (7) from a said end (11 or 13) of the line (7).

2. An equipment according to Claim 1 wherein: X_f is the voltage at the fault (9); $A_s = \cosh(Tx)$; $B_s = Z_0 \sinh(Tx)$; $A_R = \cosh(T(L-x))$ and $B_R = Z_0 \sinh(T(L-x))$, where T is the propagation constant of said line (7), x is the distance of the fault (9) along the transmission line (7) from said first end (11), Z_0 is the characteristic impedance of said line (7) and L is the total length of the line (7) between said first (11) and second (13) ends.
3. An equipment according to Claim 1 or Claim 2 wherein: said power transmission line (7) is a multi-phase power transmission line (7); said first (15A,17A,19A) and second (15B,17B,19B) means derive a set of said first, second, third and fourth signals in respect of each phase of said transmission line (7); and said means (21A,21B) for calculating includes means for transforming said signals to produce corresponding sets of decoupled signals V_{Sn} , I_{Sn} , V_{Rn} , I_{Rn} and means for utilising each set of said decoupled signals and equations of the form:

$$X_{In} = A_{Sn} V_{Sn} - B_{Sn} I_{Sn} ; \text{ and}$$

$$X_{In} = A_{Rn} V_{Rn} - B_{Rn} I_{Rn} ,$$

where n indicates the relevant said set.

4. An equipment according to Claim 3 wherein the transformation applied by said means for transforming is a modal component transformation.
5. An equipment according to any one of the preceding claims wherein said first (15A,17A,19A) and second (15B,17B,19B) means each include an analogue to digital converter (19A,19B) and said means for calculating (21A,21B) comprises a microprocessor (21A,21B).

- 10 6. A method of locating the position of a fault (9) on a power transmission line (7) between a first (11) and a second (13) end of said line (7) comprising the steps of: deriving first and second signals representative respectively of the voltage V_S and current I_S at said first end (11); deriving third and fourth signals representative respectively of the voltage V_R and current I_R at said second end (13); and calculating the position of the fault utilising said first, second, third and fourth signals and equations of the form:

$$X_f = A_S V_S - B_S I_S ; \text{ and}$$

$$X_f = A_R V_R - B_R I_R ,$$

20 where X_f is the fault voltage or current, A_S is a first transmission parameter of the line (7) between the fault (9) and said first end (11), B_S is a second transmission parameter of the line (7) between the fault (9) and said first end (11), A_R is a first transmission parameter of the line (7) between the fault (9) and said second end (13), and B_R is a second transmission parameter of the line (7) between the fault (9) and said second end (13), each said transmission parameter being dependent upon the distance of the fault (9) along the transmission line (7) from a said end (11 or 13) of the line (7).

- 25 7. A method according to Claim 6 wherein: X_f is the voltage at the fault (9); $A_S = \cosh(Tx)$; $B_S = Z_0 \sinh(Tx)$; $A_R = \cosh(T(L-x))$ and $B_R = Z_0 \sinh(T(L-x))$, where T is the propagation constant of said line (7), x is the distance of the fault (9) along the transmission line (7) from said first end (11), Z_0 is the characteristic impedance of said line (7) and L is the total length of the line (7) between said first (11) and second (13) ends.

- 30 8. A method according to Claim 6 or Claim 7 wherein: said power transmission line (7) is a multi-phase power transmission line (7); the steps of deriving said first, second, third and fourth signals comprise deriving a set of said first, second, third and fourth signals in respect of each phase of said transmission line (7); and the step of calculating includes transforming said signals to produce corresponding sets of decoupled signals V_{Sn} , I_{Sn} , V_{Rn} , I_{Rn} and utilising each set of said decoupled signals and equations of the form:

$$X_{fn} = A_{Sn} V_{Sn} - B_{Sn} I_{Sn} ; \text{ and}$$

$$X_{fn} = A_{Rn} V_{Rn} - B_{Rn} I_{Rn} ,$$

40 where, n indicates the relevant set.

- 45 9. A method according to Claim 8 wherein the transformation applied in the step of transforming is the modal component transformation.
10. A method according to any one of Claims 6 to 9 wherein said first, second, third and fourth signals are of digital form.

Patentansprüche

- 55 1. Anordnung zum Lokalisieren der Position eines Fehlers (9) auf einer Energieübertragungsleitung (7) zwischen einem ersten (11) und einem zweiten (13) Ende der Leitung (7), enthaltend: eine erste Einrichtung (15A, 17A, 19A) zum Ableiten erster und zweiter Signale jeweils zur Darstellung der Spannung V_S und des Stroms I_S am ersten Ende (11); eine zweite Einrichtung (15B, 17B, 19B) zum Ableiten dritter und viertes Signale jeweils zur Darstellung der Spannung V_R und des Stroms I_R am

zweiten Ende (13); und eine Einrichtung (21A, 21B) zum Berechnen der Position des Fehlers (9) unter Verwendung der ersten, zweiten, dritten und vierten Signale und von Gleichungen der Form:

$$X_f = A_S V_S - B_S I_S ; \text{ und}$$

$$X_f = A_R V_R - B_R I_R ,$$

worin X_f die Fehlerspannung oder der Fehlerstrom ist, A_S ein erster Übertragungsparameter der Leitung (7) zwischen dem Fehler (9) und dem ersten Ende (11) ist, B_S ein zweiter Übertragungsparameter der Leitung (7) zwischen dem Fehler (9) und dem ersten Ende (11) ist, A_R ein erster Übertragungsparameter der Leitung (7) zwischen dem Fehler (9) und dem zweiten Ende (13) ist und B_R ein zweiter Übertragungsparameter der Leitung (7) zwischen dem Fehler (9) und dem zweiten Ende (13) ist, wobei jeder der Übertragungsparameter abhängig ist vom Abstand des Fehlers (9) längs der Übertragungsleitung (7) von dem jeweils genannten Ende (11 oder 13) der Leitung (7).

- 15 2. Anordnung nach Anspruch 1, bei der: X_f die Spannung beim Fehler (9) ist; $A_S = \cosh(Tx)$; $B_S = Z_0 \cdot \sinh(Tx)$; $A_R = \cosh(T(L-x))$ und $B_R = Z_0 \cdot \sinh(T(L-x))$, worin T die Fortpflanzungskonstante der Leitung (7) ist, x der Abstand des Fehlers (9) längs der Übertragungsleitung (7) vom ersten Ende (11) ist, Z_0 der Kennwiderstand der Leitung (7) ist und L die Gesamtlänge der Leitung (7) zwischen dem ersten (11) und dem zweiten (13) Ende ist.

- 20 3. Anordnung nach Anspruch 1 oder Anspruch 2, bei der: die Energieübertragungsleitung (7) eine Mehrphasenenergie-Übertragungsleitung (7) ist; die erste (15A, 17A, 19A) und zweite (15B, 17B, 19B) Einrichtung einen Satz erster, zweiter, dritter und vierter Signale in bezug auf jede Phase der Übertragungsleitung (7) ableitet; und die Einrichtung (21A, 21B) zum Berechnen einer Einrichtung zum Umformen der Signale zum Gewinnen entsprechender Sätze entkoppelter Signale V_{Sn} , I_{Sn} , V_{Rn} , I_{Rn} und eine Einrichtung zum Verwenden jedes Satzes der entkoppelten Signale und von Gleichungen der Form enthält:

$$X_{In} = A_{Sn} V_{Sn} - B_{Sn} I_{Sn} ; \text{ und}$$

$$X_{In} = A_{Rn} V_{Rn} - B_{Rn} I_{Rn} ,$$

worin n den jeweils relevanten Satz angibt.

4. Anordnung nach Anspruch 3, bei der die Transformation, die von der Einrichtung zum Umformen angewendet wird, eine Modalkomponententransformation ist.

- 35 5. Anordnung nach irgendeinem der vorangegangenen Ansprüche, bei der die erste (15A, 17A, 19A) und zweite (15B, 17B, 19B) Einrichtung jeweils einen Analog/Digital-Umsetzer (19A, 19B) enthält und die Einrichtung zum Berechnen (21A, 21B) einen Mikroprozessor (21A, 21B) enthält.

- 40 6. Verfahren zum Lokalisieren der Position eines Fehlers (9) auf eine Energieübertragungsleitung (7) zwischen einem ersten (11) und einem zweiten (13) Ende der Leitung (7), enthaltend die Schritte: Ableiten von ersten und zweiten Signalen jeweils darstellend die Spannung V_S und den Strom I_S bei dem ersten Ende (11); Ableiten von dritten und vierten Signalen jeweils darstellend die Spannung V_R und den Strom I_R an dem zweiten Ende (13); und Berechnen der Position des Fehlers unter Verwendung der ersten, zweiten, dritten und vierten Signale und von Gleichungen der Form:

$$X_f = A_S V_S - B_S I_S ; \text{ und}$$

$$X_f = A_R V_R - B_R I_R ,$$

- 50 55 60 65 70 75 80 85 90 95 100 105 110 115 120 125 130 135 140 145 150 155 160 165 170 175 180 185 190 195 200 205 210 215 220 225 230 235 240 245 250 255 260 265 270 275 280 285 290 295 300 305 310 315 320 325 330 335 340 345 350 355 360 365 370 375 380 385 390 395 400 405 410 415 420 425 430 435 440 445 450 455 460 465 470 475 480 485 490 495 500 505 510 515 520 525 530 535 540 545 550 555 560 565 570 575 580 585 590 595 600 605 610 615 620 625 630 635 640 645 650 655 660 665 670 675 680 685 690 695 700 705 710 715 720 725 730 735 740 745 750 755 760 765 770 775 780 785 790 795 800 805 810 815 820 825 830 835 840 845 850 855 860 865 870 875 880 885 890 895 900 905 910 915 920 925 930 935 940 945 950 955 960 965 970 975 980 985 990 995 1000 1005 1010 1015 1020 1025 1030 1035 1040 1045 1050 1055 1060 1065 1070 1075 1080 1085 1090 1095 1100 1105 1110 1115 1120 1125 1130 1135 1140 1145 1150 1155 1160 1165 1170 1175 1180 1185 1190 1195 1200 1205 1210 1215 1220 1225 1230 1235 1240 1245 1250 1255 1260 1265 1270 1275 1280 1285 1290 1295 1300 1305 1310 1315 1320 1325 1330 1335 1340 1345 1350 1355 1360 1365 1370 1375 1380 1385 1390 1395 1400 1405 1410 1415 1420 1425 1430 1435 1440 1445 1450 1455 1460 1465 1470 1475 1480 1485 1490 1495 1500 1505 1510 1515 1520 1525 1530 1535 1540 1545 1550 1555 1560 1565 1570 1575 1580 1585 1590 1595 1600 1605 1610 1615 1620 1625 1630 1635 1640 1645 1650 1655 1660 1665 1670 1675 1680 1685 1690 1695 1700 1705 1710 1715 1720 1725 1730 1735 1740 1745 1750 1755 1760 1765 1770 1775 1780 1785 1790 1795 1800 1805 1810 1815 1820 1825 1830 1835 1840 1845 1850 1855 1860 1865 1870 1875 1880 1885 1890 1895 1900 1905 1910 1915 1920 1925 1930 1935 1940 1945 1950 1955 1960 1965 1970 1975 1980 1985 1990 1995 2000 2005 2010 2015 2020 2025 2030 2035 2040 2045 2050 2055 2060 2065 2070 2075 2080 2085 2090 2095 2100 2105 2110 2115 2120 2125 2130 2135 2140 2145 2150 2155 2160 2165 2170 2175 2180 2185 2190 2195 2200 2205 2210 2215 2220 2225 2230 2235 2240 2245 2250 2255 2260 2265 2270 2275 2280 2285 2290 2295 2300 2305 2310 2315 2320 2325 2330 2335 2340 2345 2350 2355 2360 2365 2370 2375 2380 2385 2390 2395 2400 2405 2410 2415 2420 2425 2430 2435 2440 2445 2450 2455 2460 2465 2470 2475 2480 2485 2490 2495 2500 2505 2510 2515 2520 2525 2530 2535 2540 2545 2550 2555 2560 2565 2570 2575 2580 2585 2590 2595 2600 2605 2610 2615 2620 2625 2630 2635 2640 2645 2650 2655 2660 2665 2670 2675 2680 2685 2690 2695 2700 2705 2710 2715 2720 2725 2730 2735 2740 2745 2750 2755 2760 2765 2770 2775 2780 2785 2790 2795 2800 2805 2810 2815 2820 2825 2830 2835 2840 2845 2850 2855 2860 2865 2870 2875 2880 2885 2890 2895 2900 2905 2910 2915 2920 2925 2930 2935 2940 2945 2950 2955 2960 2965 2970 2975 2980 2985 2990 2995 3000 3005 3010 3015 3020 3025 3030 3035 3040 3045 3050 3055 3060 3065 3070 3075 3080 3085 3090 3095 3100 3105 3110 3115 3120 3125 3130 3135 3140 3145 3150 3155 3160 3165 3170 3175 3180 3185 3190 3195 3200 3205 3210 3215 3220 3225 3230 3235 3240 3245 3250 3255 3260 3265 3270 3275 3280 3285 3290 3295 3300 3305 3310 3315 3320 3325 3330 3335 3340 3345 3350 3355 3360 3365 3370 3375 3380 3385 3390 3395 3400 3405 3410 3415 3420 3425 3430 3435 3440 3445 3450 3455 3460 3465 3470 3475 3480 3485 3490 3495 3500 3505 3510 3515 3520 3525 3530 3535 3540 3545 3550 3555 3560 3565 3570 3575 3580 3585 3590 3595 3600 3605 3610 3615 3620 3625 3630 3635 3640 3645 3650 3655 3660 3665 3670 3675 3680 3685 3690 3695 3700 3705 3710 3715 3720 3725 3730 3735 3740 3745 3750 3755 3760 3765 3770 3775 3780 3785 3790 3795 3800 3805 3810 3815 3820 3825 3830 3835 3840 3845 3850 3855 3860 3865 3870 3875 3880 3885 3890 3895 3900 3905 3910 3915 3920 3925 3930 3935 3940 3945 3950 3955 3960 3965 3970 3975 3980 3985 3990 3995 4000 4005 4010 4015 4020 4025 4030 4035 4040 4045 4050 4055 4060 4065 4070 4075 4080 4085 4090 4095 4100 4105 4110 4115 4120 4125 4130 4135 4140 4145 4150 4155 4160 4165 4170 4175 4180 4185 4190 4195 4200 4205 4210 4215 4220 4225 4230 4235 4240 4245 4250 4255 4260 4265 4270 4275 4280 4285 4290 4295 4300 4305 4310 4315 4320 4325 4330 4335 4340 4345 4350 4355 4360 4365 4370 4375 4380 4385 4390 4395 4400 4405 4410 4415 4420 4425 4430 4435 4440 4445 4450 4455 4460 4465 4470 4475 4480 4485 4490 4495 4500 4505 4510 4515 4520 4525 4530 4535 4540 4545 4550 4555 4560 4565 4570 4575 4580 4585 4590 4595 4600 4605 4610 4615 4620 4625 4630 4635 4640 4645 4650 4655 4660 4665 4670 4675 4680 4685 4690 4695 4700 4705 4710 4715 4720 4725 4730 4735 4740 4745 4750 4755 4760 4765 4770 4775 4780 4785 4790 4795 4800 4805 4810 4815 4820 4825 4830 4835 4840 4845 4850 4855 4860 4865 4870 4875 4880 4885 4890 4895 4900 4905 4910 4915 4920 4925 4930 4935 4940 4945 4950 4955 4960 4965 4970 4975 4980 4985 4990 4995 5000 5005 5010 5015 5020 5025 5030 5035 5040 5045 5050 5055 5060 5065 5070 5075 5080 5085 5090 5095 5100 5105 5110 5115 5120 5125 5130 5135 5140 5145 5150 5155 5160 5165 5170 5175 5180 5185 5190 5195 5200 5205 5210 5215 5220 5225 5230 5235 5240 5245 5250 5255 5260 5265 5270 5275 5280 5285 5290 5295 5300 5305 5310 5315 5320 5325 5330 5335 5340 5345 5350 5355 5360 5365 5370 5375 5380 5385 5390 5395 5400 5405 5410 5415 5420 5425 5430 5435 5440 5445 5450 5455 5460 5465 5470 5475 5480 5485 5490 5495 5500 5505 5510 5515 5520 5525 5530 5535 5540 5545 5550 5555 5560 5565 5570 5575 5580 5585 5590 5595 5600 5605 5610 5615 5620 5625 5630 5635 5640 5645 5650 5655 5660 5665 5670 5675 5680 5685 5690 5695 5700 5705 5710 5715 5720 5725 5730 5735 5740 5745 5750 5755 5760 5765 5770 5775 5780 5785 5790 5795 5800 5805 5810 5815 5820 5825 5830 5835 5840 5845 5850 5855 5860 5865 5870 5875 5880 5885 5890 5895 5900 5905 5910 5915 5920 5925 5930 5935 5940 5945 5950 5955 5960 5965 5970 5975 5980 5985 5990 5995 6000 6005 6010 6015 6020 6025 6030 6035 6040 6045 6050 6055 6060 6065 6070 6075 6080 6085 6090 6095 6100 6105 6110 6115 6120 6125 6130 6135 6140 6145 6150 6155 6160 6165 6170 6175 6180 6185 6190 6195 6200 6205 6210 6215 6220 6225 6230 6235 6240 6245 6250 6255 6260 6265 6270 6275 6280 6285 6290 6295 6300 6305 6310 6315 6320 6325 6330 6335 6340 6345 6350 6355 6360 6365 6370 6375 6380 6385 6390 6395 6400 6405 6410 6415 6420 6425 6430 6435 6440 6445 6450 6455 6460 6465 6470 6475 6480 6485 6490 6495 6500 6505 6510 6515 6520 6525 6530 6535 6540 6545 6550 6555 6560 6565 6570 6575 6580 6585 6590 6595 6600 6605 6610 6615 6620 6625 6630 6635 6640 6645 6650 6655 6660 6665 6670 6675 6680 6685 6690 6695 6700 6705 6710 6715 6720 6725 6730 6735 6740 6745 6750 6755 6760 6765 6770 6775 6780 6785 6790 6795 6800 6805 6810 6815 6820 6825 6830 6835 6840 6845 6850 6855 6860 6865 6870 6875 6880 6885 6890 6895 6900 6905 6910 6915 6920 6925 6930 6935 6940 6945 6950 6955 6960 6965 6970 6975 6980 6985 6990 6995 7000 7005 7010 7015 7020 7025 7030 7035 7040 7045 7050 7055 7060 7065 7070 7075 7080 7085 7090 7095 7100 7105 7110 7115 7120 7125 7130 7135 7140 7145 7150 7155 7160 7165 7170 7175 7180 7185 7190 7195 7200 7205 7210 7215 7220 7225 7230 7235 7240 7245 7250 7255 7260 7265 7270 7275 7280 7285 7290 7295 7300 7305 7310 7315 7320 7325 7330 7335 7340 7345 7350 7355 7360 7365 7370 7375 7380 7385 7390 7395 7400 7405 7410 7415 7420 7425 7430 7435 7440 7445 7450 7455 7460 7465 7470 7475 7480 7485 7490 7495 7500 7505 7510 7515 7520 7525 7530 7535 7540 7545 7550 7555 7560 7565 7570 7575 7580 7585 7590 7595 7600 7605 7610 7615 7620 7625 7630 7635 7640 7645 7650 7655 7660 7665 7670 7675 7680 7685 7690 7695 7700 7705 7710 7715 7720 7725 7730 7735 7740 7745 7750 7755 7760 7765 7770 7775 7780 7785 7790 7795 7800 7805 7810 7815 7820 7825 7830 7835 7840 7845 7850 7855 7860 7865 7870 7875 7880 7885 7890 7895 7900 7905 7910 7915 7920 7925 7930 7935 7940 7945 7950 7955 7960 7965 7970 7975 7980 7985 7990 7995 8000 8005 8010 8015 8020 8025 8030 8035 8040 8045 8050 8055 8060 8065 8070 8075 8080 8085 8090 8095 8100 8105 8110 8115 8120 8125 8130 8135 8140 8145 8150 8155 8160 8165 8170 8175 8180 8185 8190 8195 8200 8205 8210 8215 8220 8225 8230 8235 8240 8245 8250 8255 8260 8265 8270 8275 8280 8285 8290 8295 8300 8305 8310 8315 8320 8325 8330 8335 8340 8345 8350 8355 8360 8365 8370 8375 8380 8385 8390 8395 8400 8405 8410 8415 8420 8425 8430 8435 8440 8445 8450 8455 8460 8465 8470 8475 8480 8485 8490 8495 8500 8505 8510 8515 8520 8525 8530 8535 8540 8545 8550 8555 8560 8565 8570 8575 8580 8585 8590 8595 8600 8605 8610 8615 8620 8625 8630 8635 8640 8645 8650 8655 8660 8665 8670 8675 8680 8685 8690 8695 8700 8705 8710 8715 8720 8725 8730 8735 8740 8745 8750 8755 8760 8765 8770 8775 8780 8785 8790 8795 8800 8805 8810 8815 8820 8825 8830 8835 8840 8845 8850 8855 8860 8865 8870 8875 8880 8885 8890 8895 8900 8905 8910 8915 8920 8925 8930 8935 8940 8945 8950 8955 8960 8965 8970 8975 8980 8985 8990 8995 9000 9005 9010 9015 9020 9025 9030 9035 9040 9045 9050 9055 9060 9065 9070 9075 9080 9085 9090 9095 9100 9105 9110 9115 9120 9125 9130 9135 9140 9145 9150 9155 9160 9165 9170 9175 9180 9185 9190 9195 9200 9205 9210 9215 9220 9225 9230 9235 9240 9245 9250 9255 9260 9265 9270 9275 9280 9285 9290 9295 9300 9305 9310 9315 9320 9325 9330 9335 9340 9345 9350 9355 9360 9365 9370 9375 9380 9385 9390 9395 9400 9405 9410 9415 9420 9425 9430 9435 9440 9445 9450 9455 9460 9465 9470 9475 9480 9485 9490 9495 9500 9505 9510 9515 9520 9525 9530 9535 9540 9545 9550 9555 9560 9565 9570 9575 9580 9585 9590 9595 9600 9605 9610 9615 9620 9625 9630 9635 9640 9645 9650 9655 9660 9665 9670 9675 9680 9685 9690 9695 9700 9705 9710 9715 9720 9725 9730 9735 9740 9745 9750 9755 9760 9765 9770 9775 9780 9785 9790 9795 9800 9805 9810 9815 9820 9825 9830 98

7. Verfahren nach Anspruch 6, bei dem: X_f die Spannung beim Fehler (9) ist; $A_S = \cosh(Tx)$; $B_S = Z_0 \sinh(Tx)$; $A_R = \cosh(T(L-x))$ und $B_R = Z_0 \sinh(T(L-x))$, worin T die Fortpflanzungskonstante der Leitung (7) ist, x der Abstand des Fehlers (9) längs der Übertragungsleitung (7) vom ersten Ende (11) aus ist, Z_0 der Kennwiderstand der Leitung (7) ist und L die Gesamtlänge der Leitung (7) zwischen dem ersten (11) und zweiten (13) Ende ist.
8. Verfahren nach Anspruch 6 oder Anspruch 7, bei dem: die Energieübertragungsleitung (7) eine Mehrphasenenergieübertragungsleitung (7) ist, die Schritte des Ableitens der ersten, zweiten, dritten und vierten Signale das Ableiten eines Satzes der ersten, zweiten, dritten und vierten Signale in bezug auf jede Phase der Übertragungsleitung (7) umfassen; und der Schritt des Berechnens die Umformung der Signale zum Gewinnen entsprechender Sätze entkoppelter Signale V_{Sn} , I_{Sn} , V_{Rn} und I_{Rn} umfaßt sowie die Verwendung jedes Satzes der entkoppelten Signale und von Gleichungen der Form umfaßt:

15 $X_{fn} = A_{Sn}V_{Sn} - B_{Sn}I_{Sn}$; und
 $X_{fn} = A_{Rn}V_{Rn} - B_{Rn}I_{Rn}$,

worin n den relevanten Satz angibt.

9. Verfahren nach Anspruch 8, bei dem die Transformation, die beim Schritt des Umformens angewendet wird, die Modalkomponententransformation ist.
10. Verfahren nach irgendeinem der Ansprüche 6 bis 9, bei dem die ersten, zweiten, dritten und vierten Signale in digitaler Form vorliegen.

25 **Revendications**

1. Appareillage de localisation de la position d'un défaut (9) dans une ligne de transmission d'énergie (7) entre une première extrémité (11) et une seconde extrémité (13) de la ligne (7), comprenant un premier dispositif (15A, 17A, 19A) destiné à dériver des premiers et des seconds signaux représentatifs respectivement de la tension V_S et du courant I_S à la première extrémité (11), un second dispositif (15B, 17B, 19B) destiné à dériver des troisièmes et des quatrièmes signaux représentatifs respectivement de la tension V_R et du courant I_R à la seconde extrémité (13), et un dispositif (21A, 21B) destiné à calculer la position du défaut (9) par utilisation des premiers, seconds, troisièmes et quatrièmes signaux et d'équations de la forme

35 $X_f = A_S V_S - B_S I_S$,
 $X_f = A_R V_R - B_R I_R$

40 X_f étant le courant ou la tension de défaut, A_S étant un premier paramètre de transmission de la ligne (7) entre le défaut (9) et la première extrémité (11), B_S étant un second paramètre de transmission de la ligne (7) entre le défaut (9) et la première extrémité (11), A_R étant un premier paramètre de transmission de la ligne (7) entre le défaut (9) et la seconde extrémité (13), et B_R étant un second paramètre de transmission de la ligne (7) entre le défaut (9) et la seconde extrémité (13), chaque paramètre de transmission dépendant de la distance du défaut (9), le long de la ligne de transmission (7), à ladite extrémité (11 ou 13) de la ligne (7).

- 45 2. Appareillage selon la revendication 1, dans lequel X_f est la tension au niveau du défaut (9), $A_S = ch(Tx)$, $B_S = Z_0 \cdot sh(Tx)$, $A_R = ch[T(L-x)]$, et $B_R = Z_0 \cdot sh[T(L-x)]$, T étant la constante de propagation de la ligne (7), x la distance du défaut (9) le long de la ligne de transmission (7) à la première extrémité (11), Z_0 étant l'impédance caractéristique de la ligne (7), et L étant la longueur totale de la ligne (7) entre la première extrémité (11) et la seconde extrémité (13).
- 50 3. Appareillage selon la revendication 1 ou 2, dans lequel la ligne de transmission d'énergie (7) est une ligne de transmission d'énergie polyphasée (7), le premier dispositif (15A, 17A, 19A) et le second dispositif (15B, 17B, 19B) dérivent d'un ensemble des premiers, seconds, troisièmes et quatrièmes signaux pour chaque phase de la ligne de transmission (7), et le dispositif (21A, 21B) de calcul comprend un dispositif destiné à transformer les signaux pour la formation d'ensembles correspondants de signaux découplés V_{Sn} , I_{Sn} , V_{Rn} , I_{Rn} , et un dispositif destiné à utiliser chaque ensemble de

signaux découplés et des équations de la forme

$$X_{fn} = A_{Sn}V_{Sn} - B_{Sn}I_{Sn}, \text{ et}$$

$$X_{fn} = A_{Rn}V_{Rn} - B_{Rn}I_{Rn}$$

5

n indiquant l'ensemble correspondant.

4. Appareillage selon la revendication 3, dans lequel la transformation appliquée par le dispositif de transformation est une transformation des composantes modales.

10

5. Appareillage selon l'une quelconque des revendications précédentes, dans lequel le premier dispositif (15A, 17A, 19A) et le second dispositif (15B, 17B, 19B) comprennent chacun un convertisseur analogique-numérique (19A, 19B) et le dispositif de calcul (21A, 21B) comprend un microprocesseur (21A, 21B).

15

6. Procédé de localisation de la position d'un défaut (9) dans une ligne de transmission d'énergie (7) entre une première extrémité (11) et une seconde extrémité (13) de la ligne (7), comprenant les étapes suivantes : la dérivation de premiers et de seconds signaux représentatifs respectivement de la tension V_S et du courant I_S à la première extrémité (11), la dérivation de troisièmes et quatrièmes signaux représentatifs respectivement de la tension V_R et du courant I_R à la seconde extrémité (13), et le calcul de la position du défaut à l'aide des premiers, seconds, troisièmes et quatrièmes signaux et d'équations de la forme

20

$$X_f = A_S V_S - B_S I_S,$$

25

$$X_f = A_R V_R - B_R I_R$$

X_f étant le courant ou la tension de défaut, A_S étant un premier paramètre de transmission de la ligne (7) entre le défaut (9) et la première extrémité (11), B_S étant un second paramètre de transmission de la ligne (7) entre le défaut (9) et la première extrémité (11), A_R étant un premier paramètre de transmission de la ligne (7) entre le défaut (9) et la seconde extrémité (13), et B_R étant un second paramètre de transmission de la ligne (7) entre le défaut (9) et la seconde extrémité (13), chaque paramètre de transmission dépendant de la distance du défaut (9), le long de la ligne de transmission (7), à ladite extrémité (11 ou 13) de la ligne (7).

35

7. Procédé selon la revendication 6, dans lequel X_f est la tension au niveau du défaut (9), $A_S = ch(Tx)$, $B_S = Z_0.sh(Tx)$, $A_R = ch[T(L-x)]$, et $B_R = Z_0.sh[T(L-x)]$, T étant la constante de propagation de la ligne (7), x la distance du défaut (9) le long de la ligne de transmission (7) à la première extrémité (11), Z_0 étant l'impédance caractéristique de la ligne (7), et L étant la longueur totale de la ligne (7) entre la première extrémité (11) et la seconde extrémité (13).

40

8. Procédé selon la revendication 6 ou 7, dans lequel la ligne de transmission d'énergie (7) est une ligne de transmission d'énergie polyphasée (7), les étapes de dérivation des premiers, seconds et quatrième signaux comprennent la dérivation d'un ensemble de premiers, seconds, troisièmes et quatrièmes signaux pour chaque phase de la ligne de transmission (7), et l'étape de calcul comprend la transformation des signaux pour la production d'ensembles correspondants de signaux découplés V_{Sn} , I_{Sn} , V_{Rn} , I_{Rn} et l'utilisation de chacun des ensembles de signaux découplés et d'équations de la forme

45

$$X_{fn} = A_{Sn}V_{Sn} - B_{Sn}I_{Sn}, \text{ et}$$

$$X_{fn} = A_{Rn}V_{Rn} - B_{Rn}I_{Rn}$$

50

n indiquant l'ensemble correspondant.

9. Procédé selon la revendication 10, dans lequel la transformation appliquée dans l'étape de transformation est une transformation de composantes modales.

55

10. Procédé selon l'une quelconque des revendications 6 à 9, dans lequel les premiers, seconds, troisièmes et quatrièmes signaux sont sous forme numérique.

Fig.1.

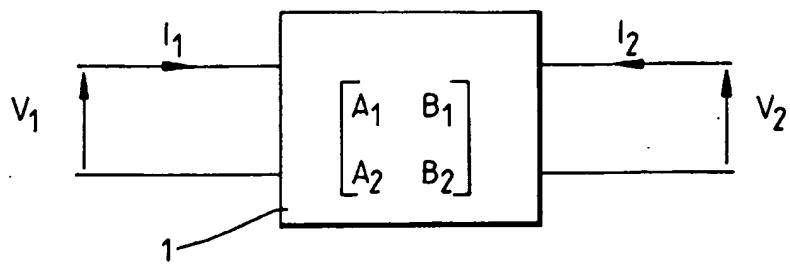


Fig.2.

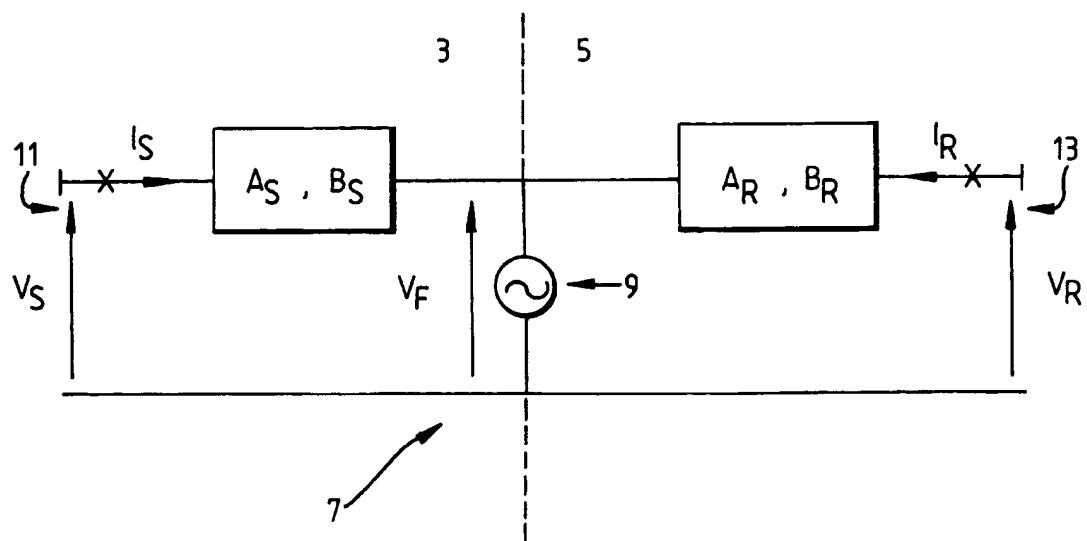


Fig.3.

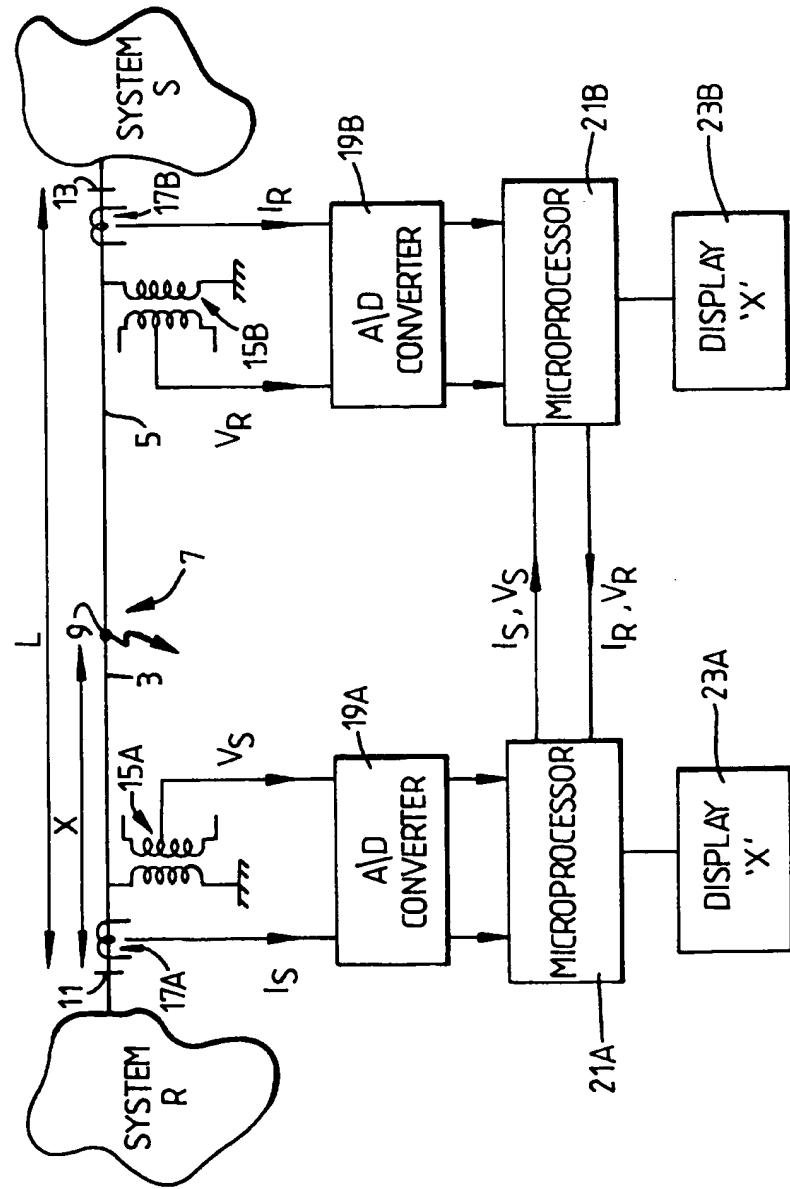


Fig.4.

